



## Letter

Phase structure and microwave dielectric properties of  $(1-x)\text{Li}_2\text{Zn}_3\text{Ti}_4\text{O}_{12}-x\text{TiO}_2$  ceramics

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## ABSTRACT

Microwave dielectric ceramics with the composition of  $(1-x)\text{Li}_2\text{Zn}_3\text{Ti}_4\text{O}_{12}$  (LZT)- $x\text{TiO}_2$  ( $0 \leq x < 1$ ) were prepared by the solid-state reaction method. The crystal structures were determined by X-ray diffraction.  $(1-x)\text{LZT}-x\text{TiO}_2$  solid solutions show a cubic structure [ $P4_332$  ( $212$ )] similar to  $\text{Zn}_2\text{Ti}_3\text{O}_8$  in the range of  $0.2 \leq x \leq 0.4$ . When the  $x$  value reaches 0.6, the rutile  $\text{TiO}_2$  phase appears. The microwave dielectric properties were studied by a Network Analyzer. The relative permittivity ( $\epsilon_r$ ) and temperature coefficients of resonant frequency ( $\tau_f$ ) were adjusted with increasing  $x$  values. Especially,  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramic exhibits good microwave dielectric properties with a  $\epsilon_r$  of 25.1, a high  $Q \times f$  of 62,000 GHz and a near-zero  $\tau_f$  of  $-5.2$  ppm/ $^\circ\text{C}$ .

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## 1. Introduction

The recent progress in microwave telecommunication, satellite broadcasting and intelligent transport systems (ITS) has resulted in an increasing demand for dielectric resonators (DRs). Dielectric resonators generally consist of a puck of ceramic that has high permittivity and low dissipation factor. The resonant frequency of a DR is determined by the overall physical dimensions of the puck, the permittivity of the material and its immediate surroundings. The key properties are high-quality factor ( $Q$ ), high relative permittivity ( $\epsilon_r$ ) and near-zero temperature coefficient of resonant frequency ( $\tau_f$ ). However, an optimal DR that satisfies these three properties simultaneously is difficult to achieve in a particular material [1–3].

Recently, a number of microwave dielectric ceramics have been developed, such as  $\text{Ca}(\text{B}'_{1/2}\text{Nb}_{1/2})\text{O}_3$  [ $\text{B}' = \text{La, Pr, Nd, Sm, Eu, Gd, Tb, Y, Er, Yb}$  and  $\text{In}$ ] [4] and  $\text{MAl}_2\text{O}_4$  ( $\text{M} = \text{Zn}$  and  $\text{Mg}$ ) [5–7]. However, most of these ceramics have a large negative  $\tau_f$  value. Generally, there are two methods to design a material with a stable temperature coefficient: (1) composite materials by mixing component materials [8] with negative and positive  $\tau_f$  values, such as  $\text{Zn}_2\text{Te}_3\text{O}_8-\text{TiO}_2$  [9],  $\text{Zn}_2\text{TiO}_4-\text{TiO}_2$  [10],  $\text{Ca}_2\text{P}_2\text{O}_7-\text{TiO}_2$  [11],  $\text{CaWO}_4-\text{TiO}_2$  [12],  $\text{Mg}_4\text{Ta}_2\text{O}_9-\text{TiO}_2$  [13] and  $\text{LiNb}_3\text{O}_8-\text{TiO}_2$  [14]. (2) Formation of solid solutions, such as complex perovskites [15] and other systems [16–17]. More recently, Wu et al. [18] reported temperature

stable microwave dielectric ceramic  $0.3\text{Li}_2\text{TiO}_3-0.7\text{Li}(\text{Zn}_{0.5}\text{Ti}_{1.5})\text{O}_4$  with ultra-low dielectric loss by composite method. In our recent investigation,  $\text{ZnLi}_{2/3}\text{Ti}_{4/3}\text{O}_4$  ceramic presents excellent microwave dielectric properties with  $\epsilon_r = 20.6$ ,  $Q \times f = 106,700$  GHz,  $\tau_f = -48$  ppm/ $^\circ\text{C}$  [19]. In order to enhance the  $\epsilon_r$  and  $\tau_f$  values, rutile  $\text{TiO}_2$  ( $\epsilon_r = 105$ ,  $Q \times f = 46,000$  GHz,  $\tau_f = +465$  ppm/ $^\circ\text{C}$ ) [20] was added to the LZT ceramic. In this work, sintering characteristics, phase structure and microwave dielectric properties of  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics have been investigated.

## 2. Experimental

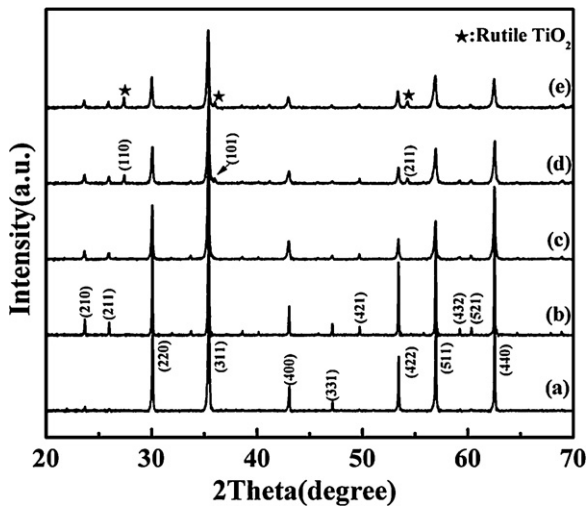
In order to synthesize LZT powders, high-purity powders of  $\text{Li}_2\text{CO}_3$  ( $\geq 99\%$ , Guo-Yao Co. Ltd., Shanghai, China),  $\text{ZnO}$  ( $\geq 99\%$ , Guo-Yao Co. Ltd., Shanghai, China) and  $\text{TiO}_2$  ( $\geq 99\%$ , Guo-Yao Co. Ltd., Shanghai, China) were weighed according to the molar ratio of 1:3:4. The mixture was ball-milled in a polyethylene bottle with  $\text{ZrO}_2$  media for 4 h using alcohol as a medium. The wet mixture was rapidly dried and then calcined at  $950^\circ\text{C}$  for 6 h. Afterward, mixtures of the  $(1-x)\text{LZT}-x\text{TiO}_2$  powders ( $x = 0.2, 0.4, 0.6$  and  $0.8$ ) were ball-milled in a polyethylene bottle with  $\text{ZrO}_2$  media for 4 h using alcohol as a medium. The milled powders were dried, granulated and pressed into cylinders of 12 mm in diameter and 6–8 mm in height by uniaxial pressing under a pressure of 200 MPa. The samples were heated at  $550^\circ\text{C}$  for 4 h to remove the organic binder and then sintered at  $1050-1175^\circ\text{C}$  for 4 h at a heating rate of  $5^\circ\text{C}/\text{min}$ .

The bulk density of the sintered samples was measured by Archimedes method. The phase structure of samples was investigated by using X-ray diffractometer (XRD) ( $\text{CuK}\alpha_1$ ,  $1.54059 \text{ \AA}$ , Model X'Pert PRO, PANalytical, Almelo, Holland). The surface micrographs of the samples were examined by using a scanning electron microscope (SEM, Model JSM6380-LV, JEOL, Tokyo, Japan).

Dielectric behaviors in microwave frequency were measured by the  $\text{TE}_{018}$  shielded cavity method using a Network Analyzer (Model N5230A, Agilent Co., Palo Alto, CA) and a temperature chamber (Delta 9039, Delta Design, San Diego, CA).

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**Fig. 1.** XRD profiles for the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$  for 4 h: (a)  $x=0$ , (b)  $x=0.2$ , (c)  $x=0.4$ , (d)  $x=0.6$  and (e)  $x=0.8$ .

The temperature coefficients of resonant frequency  $\tau_f$  values were calculated by the formula as in the following:

$$\tau_f = \frac{f_T - f_0}{f_0(T - T_0)} \quad (1)$$

where  $f_T, f_0$  were the resonant frequencies at the measuring temperature  $T$  ( $85^\circ\text{C}$ ) and  $T_0$  ( $25^\circ\text{C}$ ), respectively.

### 3. Results and discussion

Fig. 1 shows the X-ray diffraction (XRD) profiles of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ( $x=0, 0.2, 0.4, 0.6$  and  $0.8$ ) samples sintered at  $1075^\circ\text{C}$  for 4 h. Pure LZT has a cubic structure [ $Fd-3m(227)$ ] similar to  $\text{MgFe}_2\text{O}_4$  with lattice parameters of  $a=8.401(7)\text{\AA}$ ,  $V=593.07\text{\AA}^3$ ,  $\rho=4.43\text{ g/cm}^3$  and  $Z=8$  ( $Z$  denotes the number of unit cell molecules in a unit cell) [19]. However, as  $x$  value is over 0.2, the added reflection peaks with  $(210)$ ,  $(211)$ ,  $(421)$ ,  $(432)$  and  $(521)$  show lower symmetry of crystal structure.  $(1-x)\text{LZT}-x\text{TiO}_2$  solid solution ( $0.2 \leq x \leq 0.4$ ) has a cubic structure [ $P4_332(212)$ ] similar to  $\text{Zn}_2\text{Ti}_3\text{O}_8$  (JCPDS #087-1781). At the region of  $x \geq 0.6$ , rutile  $\text{TiO}_2$  phase (JCPDS #071-0650) was observed, and the amount of rutile  $\text{TiO}_2$  phase increases with increasing the  $x$  values. The phase composition, crystallographic parameters of  $(1-x)\text{LZT}-x\text{TiO}_2$  ( $0 \leq x < 1$ ) ceramics sintered at  $1075^\circ\text{C}$  are shown in Table 1. The structure changes from [ $Fd-3m(227)$ ] to [ $P4_332(212)$ ], and the lattice constant decreased from  $8.401(7)\text{\AA}$  to  $8.393(6)\text{\AA}$ . However, the calculated density increased from  $4.43\text{ g/cm}^3$  (at  $x=0$ ) to  $4.84\text{ g/cm}^3$  (at  $x=0.4$ ), which was attributed to the trace change in cell volume and the increase of molar mass caused by that  $\text{Ti}^{4+}$  in titanium dioxide entered the unit cell. At the region of  $x \geq 0.6$ , rutile  $\text{TiO}_2$  phase was observed, and the mass percentage of the rutile  $\text{TiO}_2$  phase increased from 12.5% (at  $x=0.6$ ) to 30.6% (at  $x=0.8$ ) (calculated via the RIR method in the jade 6.0 software).

**Table 1**  
Phase composition and crystallographic parameters of  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$ .

$x$ values	Phase composition	Secondary phase wt (%)	Crystallographic parameters		
			Lattice constant, $a$ ( $\text{\AA}$ )	Volume of cell, $V$ ( $\text{\AA}^3$ )	Calculated density, $\rho$ ( $\text{g/cm}^3$ )
$x=0$	Single	–	8.401(7)	593.07	4.43
$x=0.2$	Single	–	8.393(6)	591.35	4.59
$x=0.4$	Single	–	8.395(8)	591.82	4.84
$x=0.6$	Mixture	$\text{TiO}_2$ : 12.5%	–	–	–
$x=0.8$	Mixture	$\text{TiO}_2$ : 30.6%	–	–	–

The microstructure of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics was observed using scanning electron microscopy (SEM). Fig. 2 illustrates SEM images of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$ . The well-densified microstructures were obtained and little porosity was observed in the sintered samples. The pure LZT ceramic [Fig. 2(a)] has a dense microstructure with the average grain size of  $\sim 50\text{ }\mu\text{m}$ . The grain size becomes smaller with increasing  $\text{TiO}_2$  contents, which may be contributed by its high sintering temperature (above  $1300^\circ\text{C}$ ). In particular, a small amount of tetragonal rutile  $\text{TiO}_2$  were firstly observed in Fig. 2(d) (at  $x=0.6$ ), which agree well with the analysis of X-ray diffraction patterns. As the  $x$  value is 0.8, the rod-like  $\text{TiO}_2$  grains with a width size of about  $2\text{ }\mu\text{m}$  and square grains with a size of about more than  $5\text{ }\mu\text{m}$  were observed [as shown in Fig. 2(e)].

The bulk density,  $Q \times f$  values and relative permittivity of the  $(1-x)\text{LZT}-x\text{TiO}_2$  samples as a function of the sintering temperatures are shown in Fig. 3. The bulk densities initially increase with increasing  $x$  values from 0.2 to 0.6 and then slightly decrease with further increasing the  $x$  values. The increase of the bulk densities can be explained by the produce of phase with higher crystallographic calculated density (as shown in Table 1). In addition, the decrease of the densities may be the emergence of excessive  $\text{TiO}_2$  with relatively lower density ( $4.25\text{ g/cm}^3$ ) as well as the reduction of the sintering characteristics of the LZT ceramics due to the high sintering temperature of  $\text{TiO}_2$  (above  $1300^\circ\text{C}$ ). It is noticeable that the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics have a relatively wide sintering temperature range (above  $100^\circ\text{C}$ ), which can be illustrated by the trace change in densities for the whole sintering temperatures. The relative permittivity increases with increasing  $x$  values. The effect of sintering temperature on the permittivity is not obvious for the same composition, which is consistent with the little change of the bulk density of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics for the same  $x$  value at different temperatures. The  $Q \times f$  values decreased with increasing  $x$  values when the sintering temperatures are lower than  $1075^\circ\text{C}$ . However, the  $Q \times f$  values initially decreased between  $x=0.2$  and 0.6 and then increased between  $x=0.6$  and 0.8 when the sintering temperatures are higher than  $1100^\circ\text{C}$ . At the region of  $0.4 \leq x \leq 0.6$ , the decrease of the  $Q \times f$  values at different sintering temperature was resulted from the produce of the  $\text{TiO}_2$  phase. Overall, the optimal sintering temperature of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics ( $x \leq 0.6$ ) is  $1075^\circ\text{C}$ .

Fig. 4 shows the temperature coefficients of resonant frequency  $\tau_f$  of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$ , insert shows the  $\tau_f$  values of the  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramics as a function of the sintering temperatures. The  $\tau_f$  values increase slightly in the  $x$  range of  $0.2 \leq x \leq 0.4$ , which may be attributed to the trace change in the crystal structure. However, due to the secondary phase  $\text{TiO}_2$ , the  $\tau_f$  values shift sharply in the range of  $0.4 < x \leq 0.8$ . Especially, when  $x$  value reach to 0.6, the  $\tau_f$  values is near to zero, which is attributed to appropriate amount of  $\text{TiO}_2$  with very high  $\tau_f$  value ( $\sim +465\text{ ppm/}^\circ\text{C}$ ) [20]. The  $\tau_f$  values of the  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramics at different sintering temperatures have no obvious change and keep relatively steady. Hence, the  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$  have excellent microwave dielectric properties with a  $\epsilon_r$  of 25.1, a high  $Q \times f$  of 62,000 GHz and a  $\tau_f$  of  $-5.2\text{ ppm/}^\circ\text{C}$ .

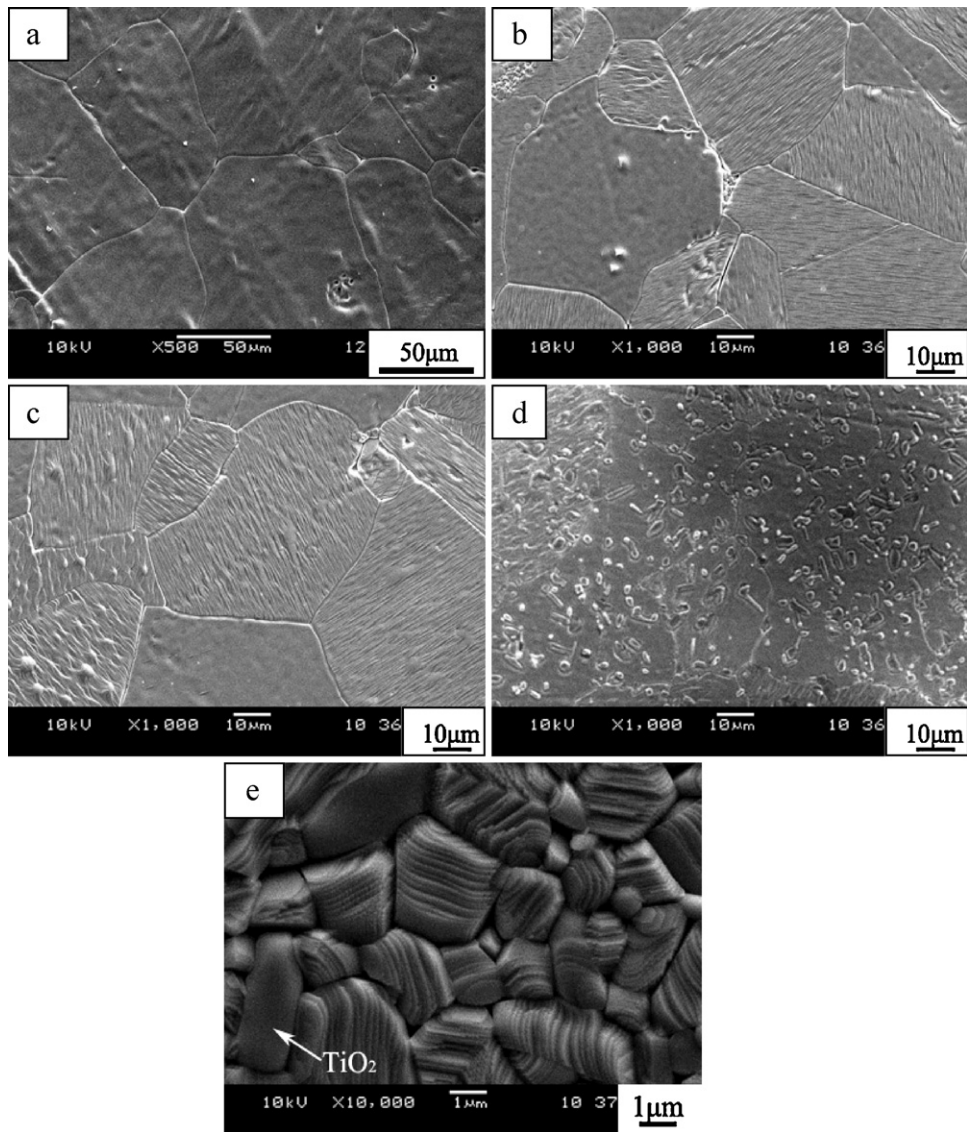


Fig. 2. The SEM micrographs of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$ : (a)  $x=0$ , (b)  $x=0.2$ , (c)  $x=0.4$ , (d)  $x=0.6$  and (e)  $x=0.8$ .

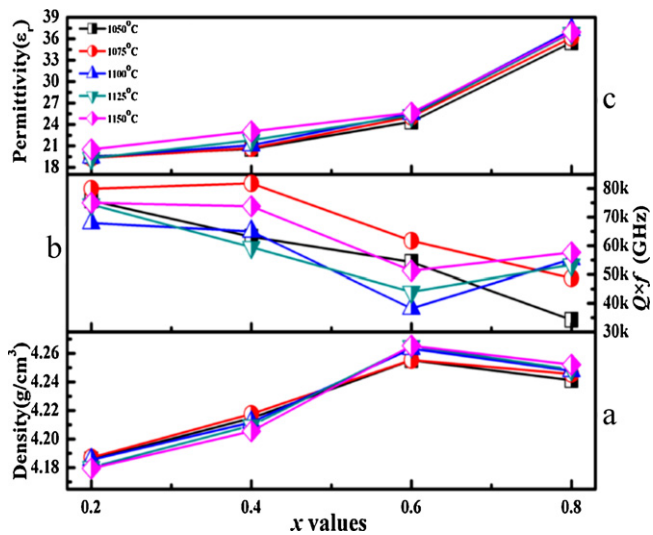


Fig. 3. The bulk density (a),  $Q \times f$  (b) and relative permittivity (c) of  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics as a function of the sintering temperature.

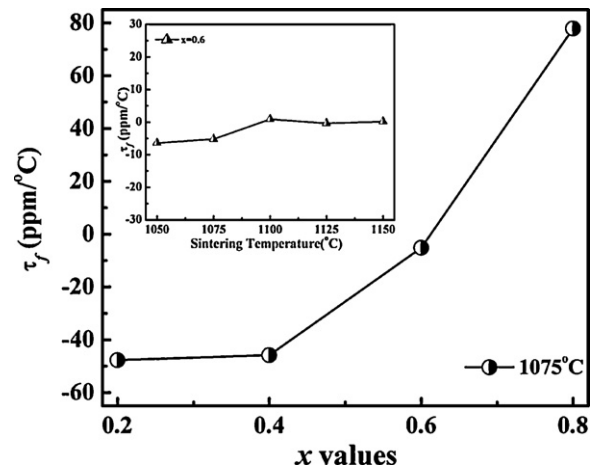


Fig. 4. The  $\tau_f$  values of  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics sintered at  $1075^\circ\text{C}$  as a function of the  $\text{TiO}_2$  content. The inset shows  $\tau_f$  values of the  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramics as a function of the sintering temperatures.

#### 4. Conclusion

In this study, the structure and microwave dielectric properties of the  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics were investigated.  $(1-x)\text{LZT}-x\text{TiO}_2$  ( $x \geq 0.2$ ) has a cubic structure  $[P4_332 (212)]$  similar to  $\text{Zn}_2\text{Ti}_3\text{O}_8$ , the rutile  $\text{TiO}_2$  phase appeared as  $x$  values are over 0.6.  $(1-x)\text{LZT}-x\text{TiO}_2$  ceramics exhibited good dielectric properties. Especially,  $0.4\text{LZT}-0.6\text{TiO}_2$  ceramic has excellent microwave dielectric properties with a  $\epsilon_r$  of 25.1, a high  $Q \times f$  of 62,000 GHz and a near-zero  $\tau_f$  of  $-5.2 \text{ ppm}/^\circ\text{C}$ .

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